# This Page Is Inserted by IFW Operations and is not a part of the Official Record

## **BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

## > IMAGES ARE BEST AVAILABLE COPY.

As rescanning documents will not correct images, please do not report the images to the Image Problem Mailbox.





(11) **EP 1 188 898 A2** 

(12)

#### **EUROPEAN PATENT APPLICATION**

(43) Date of publication: 20.03.2002 Bulletin 2002/12

(51) Int Cl.7: **E21B 10/56** 

(21) Application number: 01127883.5

(22) Date of filing: 10.10.1997

(84) Designated Contracting States: **BE DE** 

(30) Priority: 11.10.1996 GB 9621217

(62) Document number(s) of the earlier application(s) in accordance with Art. 76 EPC: 97308021.1 / 0 841 463

(71) Applicant: CAMCO DRILLING GROUP LIMITED Stonehouse, Gloucestershire GL10 3RQ (GB)

(72) Inventors:

 Taylor, Malcolm Roy Gloucester (GB)

- Griffin, Nigel Dennis Whitminster, Gloucester (GB)
- Roberts, Tom Scott Quedgeley, Gloucester (GB)
- (74) Representative: Bailey, Richard Alan
   A.R. Davies & Co.,
   27 Imperial Square
   Cheltenham, Gloucestershire GL50 1RQ (GB)

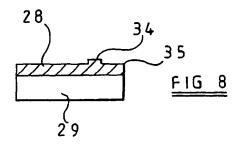
#### Remarks:

This application was filed on 23-11-2001 as a divisional application to the application mentioned under INID code 62.

### (54) Improvements in or relating to preform cutting elements for rotary drill bits

(57) A preform cutting element for a rotary drag-type drill bit comprises a front facing table (28) of superhard material having a front surface, a peripheral surface, a rear surface bonded to a substrate (29) of less hard material, and a cutting edge (35) formed by at least part of the junction between the front surface and the peripheral surface. The front surface of the facing table is formed

with a chip-breaking formation which is located adjacent the cutting edge and is shaped to deflect transversely of the front surface of the facing table cuttings which, in use, are removed by the cutting edge from the formation being drilled. The chip-breaking formation comprises a projection (34) which upstands from the front surface of the facing table.



#### Descripti n

[0001] The invention relates to preform cutting elements for rotary drag-type drill bits, for use in drilling or coring holes in subsurface formations, and of the kind comprising a bit body having a shank for connection to a drill string, a plurality of cutting elements mounted at the surface of the bit body, and a passage in the bit body for supplying drilling fluid to the surface of the bit body for cooling and/or cleaning the cutters. Each cutting element comprises a front facing table of superhard material bonded to a less hard substrate.

[0002] The cutting element may be mounted on a carrier, also of a material which is less hard than the superhard material, which is mounted on the body of the drill bit, for example, is secured within a socket on the bit body. Alternatively, the cutting element may be mounted directly on the bit body, for example the substrate may be of sufficient axial length that it may itself be secured within a socket on the bit body.

[0003] In drag-type drill bits of this kind the bit body may be machined from metal, usually steel, and sockets to receive the carriers or the cutting elements themselves are machined in the bit body. Alternatively, the bit body may be moulded from tungsten carbide matrix material using a powder metallurgy process.

[0004] Drag-type drill bits of this kind are particularly suitable for drilling softer formations. However, when drilling soft, sticky shale formations in a water based mud environment, and in other similar conditions, there may be a tendency for the shavings or chips of formation gouged from the surface of the borehole not to separate from the surface and to be held down on the surface of the formation by the subsequent passage over the shaving or chip of other cutters and parts of the drill bit. Also, there may be a tendency for such material to adhere to the surface of the bit body, a phenomenon known as "bit balling", eventually resulting in the bit becoming ineffective for further drilling.

[0005] In order to alleviate or overcome this problem, the facing table may be formed with a chip breaker which serves to break the shaving or chip of formation into fragments as it passes over the front surface of the cutting element, thus enabling the particles to be entrained in the flow of drilling fluid, and swept away from the cutting element, so that they are not held down on the formation or do not adhere to the bit.

[0006] The present invention sets out to provide improved forms of chip breakers for preform cutting elements for rotary drag-type drill bits.

[0007] According to the invention there is provided a preform cutting element for a rotary drag-type drill bit, comprising a front facing table of superhard material having a front surface, a peripheral surface, a rear surface bonded to a substrate of less hard material, and a cutting edge formed by at least part of the junction between the front surface and the peripheral surface, the front surface of the facing table being formed with a for-

mation which is located adjacent at least a part of the cutting edge and is shaped to deflect transversely of the front surface of the facing table cuttings which, in use, are removed by the cutting edge from the formation being drilled, the formation comprising at least one protrusion which upstands from the front surface.

[0008] The cutting element may be circular or part-circular in shape and said formation may extend around part or all of an outer marginal portion of the front surface of the facing table.

[0009] In one embodiment of the invention said formation further comprises a groove formed in said front surface of the facing table adjacent the cutting edge. The groove may have an outer edge which is spaced inwardly from the cutting edge. The outer edge of the groove is preferably spaced a substantially constant distance from the cutting edge. The protrusion is defined between the groove and the cutting edge.

[0010] The groove may be smoothly and concavely curved in cross-section. For example, it may be part-circular in cross-section. Alternatively, the groove may be V-shaped in cross-section, or of any other cross-sectional shape.

[0011] There may be formed in the groove a plurality of protrusions spaced apart longitudinally of the groove. Each protrusion may have an upper surface which lies at substantially the same level as the front surface of the facing table. Each protrusion may extend transversely across the groove, for example across substantially the full width of the groove. Each protrusion may be elongate and inclined at an angle of 90°, or less than 90°, to the length of the groove.

[0012] All the protrusions may be inclined at substantially the same angle to the length of the groove, or adjacent protrusions may be inclined at opposite and equal angles to the length of the groove. Each protrusion may be straight or curved as it extends across the groove. In an alternative arrangement, each protrusion is generally circular in cross-section.

0 [0013] A portion of the front surface of the facing table between the groove and the cutting edge is configured to upstand from that surface. For example, said portion of the surface may be formed with upstanding serrations. Said serrations may fill the space between the outer edge of the groove and the cutting edge, the cutting edge then being defined by parts of said serrations.

[0014] The protrusion may comprise a ridge formed on said front surface adjacent the cutting edge. The ridge may have an outer edge which is spaced inwardly from the cutting edge. The outer edge of the groove is preferably spaced a substantially constant distance from the cutting edge. The ridge may, for example be rectangular or curved in cross-section.

[0015] In any of the above embodiments said formation on the front surface of the facing table may be formed during formation of the superhard facing table in a high pressure, high temperatur press.

[0016] Alternatively, the formation may be formed on

the facing table by a shaping operation carried out subsequent to formation of the superhard facing table.

[0017] In a still further embodiment of the invention, the formation on the front surface of the facing table may be provided by an insert which is received in a socket in the cutting element adjacent the cutting edge thereof, the insert including a part which is upstanding from the front surface of the facing table.

[0018] The insert and socket may be substantially circular in cross-section. At least the part of the insert which is received in the socket may be cylindrical. The socket and insert may extend through substantially the whole thickness of the cutting element.

[0019] The upstanding part of the insert may be domed, and the outer periphery of the dome preferably lies at the same level as the front surface of the facing table.

[0020] Alternatively, the upstanding part of the insert may have a front surface which is inclined away from the front surface of the facing table as it extends away from the cutting edge. The edge of said inclined surface nearest the cutting edge of the facing table preferably lies at the same level as the front surface of the facing table.

[0021] The insert may comprise a front layer of superhard material bonded to a substrate of less hard material, the superhard material forming the front surface of the upstanding part of the insert.

[0022] The following is a detailed description of embodiments of the invention, reference being made to the accompanying drawings in which:

Figures 1-8 are diagrammatic sectional views through various forms of preform cutting element in accordance with the invention,

Figure 9 is a diagrammatic perspective view of an alternative form of element,

Figure 10 is a cross section through the cutting element of Figure 9,

Figures 11 to 13 are similar sectional views of further forms of cutting element,

Figure 14 is a diagrammatic section, on an enlarged scale, through a chip breaker groove, cutting element.

Figures 15 to 19 are plan views of cutting elements incorporating chip breakers,

Figure 20 is a part-section through a further cutting element incorporating a chip breaker,

Figure 21 is a diagrammatic part perspective view of the cutter of Figure 20,

Figures 22 and 23 are perspective views of still further forms of cutting element,

Figures 24 and 25 are diagrammatic sectional views through still further forms of cutting element, and

Figure 26 is a plan view of a component used in the manufacture of the cutting elements of Figures 24 and 25.

[0023] Figure 1 shows in cross-section part of a circular preform cutting element for a rotary drag-type drill bit. The cutting element comprises a front facing table 10 of polycrystalline diamond bonded, in a high pressure, high temperature press, to a substrate 11 of less hard material, such as cemented tungsten carbide. The manner of manufacture of preform cutting elements of this general kind are well known and will not therefore be described in detail.

[0024] As is also well known, the cutting element may be mounted on a bit body by the substrate 11 being directly received and secured within a socket in the bit body. The element may be secured, for example, by brazing or by shrink fitting. Alternatively, the substrate 11 may be brazed to a carrier, which may be in the form of a part-cylindrical stud or post, which is then in turn brazed or shrink-fitted in an appropriately shaped socket in the bit body.

[0025] An exposed part of the periphery of the facing table 10 forms a cutting edge 12 which engages the formation 13 during drilling.

[0026] Polycrystalline diamond cutting elements of this kind are generally set on the drill bit so that the front cutting face 14 of the cutting element is at 15°-20° negative back rake. That is to say the front surface 14 leans forwards in the direction of movement of the cutter as it acts on the formation. While this is suitable for the majority of formations, it may be advantageous for the front face of the cutting element to be inclined at a positive rake angle since this may cause the soft formation to shear more easily. Figure 1 shows an arrangement where this may be achieved automatically without the necessity of changing the drill bit.

[0027] For this purpose the front face 14 of the diamond facing table 10 is formed with a concave chip breaker groove 15 which extends around or across part of the marginal portion of the facing table adjacent the cutting edge 12 and spaced inwardly a short distance from the cutting edge.

[0028] When cutting harder formations the cutting edge penetrates only a short distance into the formation and the active portion of the front face 14 is therefore the small portion 16 between the cutting edge 12 and the chip breaker groove 15 which, as shown, is arranged at a negative back rake angle of 15°-20°. However, if a softer formation is encountered the cutting edge 12 will penetrate more deeply into the formation with the result that a proportion of the depth of the formation will bear against that part 17 of the groove 15 which is nearest to the cutting edge and which is arranged at a positive rake angle of 15°-30°. This provides the more aggressive shearing action appropriate for a softer formation.

[0029] At the same time, of course, the part of the groove 15 which is further from the cutting edge 12 serves as a chip breaker, causing br ak up of shavings or chips cut from the formation as they pass upwardly over the front of the cutting element. The broken up chips are then more easily dispersed in the drilling fluid

20

which will normally be flowing under pressure over the cutting element as drilling progresses, and will thus be prevented from adhering to the drill bit or being held down against the formation.

[0030] In the arrangement of Figure 1 the facing table 10 is thicker than the maximum depth of the groove 15. In the alternative arrangement in Figure 2 the substrate 18 has a shaped surface 19 to which the diamond facing table 20 is applied and the chip breaker groove 21 in the facing table corresponds to a similar groove 22 in the face 19 of the substrate, so that the facing table 20 is of substantially constant thickness.

[0031] In the arrangement of Figure 3 the polycrystalline diamond facing table 23 is formed with a cylindrical chip breaker groove 24 so that, as a shaving or chip is lifted from the formation by the cutting element it passes upwardly across the front face of the groove 24 and the curved surface tends to cause it to break into fragments. The particles can be readily washed away by the drilling fluid

[0032] In this arrangement, however, the part of the facing table 23 and substrate 25 to the rear of the cutting edge 26 are chamfered as indicated at 27, for example is conically chamfered, to provide a shallow relief angle to reduce the frictional engagement between the cutting element and the formation behind the cutting edge 26. [0033] Figures 4-8 show other configurations of the facing table 28, bonded to a tungsten carbide substrate 29 to form a chip breaker.

[0034] In the arrangement of Figure 4 the chip breaker is a rectangular section peripheral groove or rebate 30. In Figure 5 it is a concave peripheral rebate 31. In Figure 6 the chip breaker groove has a stepped section as indicated at 32. Figure 7 shows an arrangement where the chip breaker is in the form of a central saucershaped recess 33 in the front face of the facing table. Figure 8 shows an arrangement where a chip breaker comprises an upstanding bar 34 on the front face of the facing table 28. The bar 34 may be straight or may be curved so as to be generally parallel to the curved cutting edge 35 of the cutting element. The bar 34 may be formed by grinding the front surface of the facing table 28 or it may be sinter moulded on the front face of the facing table during manufacture.

[0035] In the arrangements of Figures 4-8, and indeed in any chip breaker formation on a polycrystalline diamond cutting element, chemical vapour deposition (CVD) technology may be used to apply, for example, a TiN coating to the front surface of the facing table, including the chip breaker formation, to reduce friction and chemical affinity, so as to further reduce any tendency for chips of formation to adhere to the cutting element.

[0036] In all of the arrangements described above the chip breaker formation has been in the form of a continuous groove or rebate. Figures 9 and 10 show a further arrangement, in accordance with the invention, where a peripheral chip breaker groove 36 on the facing table 37 of a cutting element is formed with a plurality of equal-

ly spaced radial ridges 38 extending across the groove 36. These ridges modify the shape and direction of the chip of formation as it passes across the chip breaker groove and aids bit cleaning.

[0037] Figure 11 shows an alternative arrangement where the chip breaker groove 39 is spaced radially inwardly from the cutting edge 40 of the facing table. In this case also radially extending ridges 41 are spaced apart around the annular groove 39.

[0038] Figure 13 shows a further arrangement in which the chip breaker groove 42 is V-shaped in cross section and is formed with radial spaced ridges 43. In this case the facing table 44 is of substantially constant thickness, the chip breaker groove 42 in the facing table lying opposite a similar V-shaped groove 45 formed in the surface of the substrate 46.

[0039] In the arrangement of Figure 12 the chip breaker comprises a circle of bumpy protrusions 47 on the front face 48 of the facing table 49, the protrusions being spaced inwardly from the peripheral cutting edge of the facing table. As in the arrangement of Figure 8, the protrusions may be formed by grinding the facing table or by forming the protrusions by sintering when the cutting element is manufactured.

[0040] In any of the arrangements of Figures 4-13, the chip break grooves may also be formed by plunge EDM. [0041] Figure 14 shows on an enlarged scale a concave chip breaker groove 50 in the facing table 51 of a cutting element where protrusions or bumps 52 are formed over the surface of the groove 50 to reduce friction between the chip and the groove as it passes over the surface of the groove.

[0042] In the arrangements of Figures 9-13, the ridges in the chip breaker groove are described as being radial. Figures 15-19 are plan views of other forms of cutting element where the ridges are of different shapes and orientations so as to control the passage of chips of formation as they pass over the groove from the cutting edge.

[0043] In the arrangement of Figure 15 the annular chip breaker groove 53 is formed with spaced transverse ridges 54 which are inclined at an angle to a radius of the cutting element which passes through each ridge. The angled ridges cause deviation of the chips of formation in a peripheral direction as the chips pass across the face of the cutting element, as indicated by the arrows 55. This further breaks up the chippings.

[0044] The breaking up of the chippings is also enhanced by the arrangement of Figure 16 where alternate ridges 56 in the annular chip breaker groove 57 are inclined in opposite directions.

[0045] Figure 17 shows a construction where chippings of formation are further broken up, and friction is reduced, by domed protrusions 58 spaced apart around the chip breaker groove 59.

[0046] The arrangement of Figure 18 is somewhat similar to that of Figure 15, but in this case the transverse ridges 60 are curved as well as being angled as

20

they extend inwardly from the cutting edge of the element.

[0047] Figure 19 shows a further modified arrangement in which the ridges 61 have a double curvature.

[0048] In the arrangements of Figures 15, 16, 18 and 19 the angled protrusions in the chip-breaking groove can serve to control the direction taken by the cuttings as they are broken from the formation.

[0049] Protrusions of the kind shown in Figures 15-19 may also be provided in the rebate 36 in the arrangement of Figures 9 and 10. Similarly the radial protrusions 38 in Figures 9 and 10 may be used in the grooves of arrangements, similar to Figures 15-19, where the groove is spaced inwardly from the cutting edge.

[0050] Figures 20 and 21 show a further chip breaker arrangement where the basic chip breaker groove 62, similar to the groove in the Figure 2 arrangement, is supplemented by a toothed or serrated lip 63 outwardly of the peripheral groove 62 and forming a serrated cutting edge for the facing table 64 of the cutting element.

[0051] In all of the above arrangements where there is provided a single chip breaker groove adjacent the cutting edge of the cutting element, the chip breaker will only be fully effective when the cutting element is new and will increasingly lose its effectiveness as a wear flat forms on the cutting element.

[0052] Figure 22 shows an arrangement where the front face 65 of the facing table of the cutting element is formed with a stepped rebate 66, 67 and 68 extending away from the cutting edge 69. When the cutting element is new the outermost step 66 performs the bulk of the chip breaking function, but as the element wears, and the portion carrying the step 66 wears away, the next inner step 67 takes over the chip breaking function, and so on. Preferably the steps are slightly curved, as shown, to match the profile of the adjacent formation formed by a number of similar cutting elements side-by-side and overlapping.

[0053] The multi-stepped arrangement of Figure 22 is also particularly advantageous for use in interbedded formations, since the steps can break up cuttings over a wide range of penetration rates.

[0054] In the construction of Figure 23, the polycrystalline diamond facing table 70 of the cutting element is formed with a two-lobed rebate 71 to provide an upstanding land 72 on the surface which is generally in the shape of a snow plough. The curved edges 73 of the land are so located and shaped that a chipping of formation cut by the cutting edge 74 passes across the rebate 71 and is split and diverted in two opposing directions by the land 72, and is thus broken up and prevented from adhering to the cutting element.

[0055] In Figure 24 a preform cutting element 75 is formed with a through-hole 76 of circular or other cross sectional shape in which is brazed an insert 77 having a domed outer surface 78. The insert 77 is of the same general construction as the main part of the cutting element, comprising a polycrystalline diamond facing table

79 bonded to a tungsten carbide substrate portion 80. Alternatively, the insert 77 may be formed from plain tungsten carbide alone. The combination cutting element is shown brazed to a carrier 81.

[0056] The insert 80, which is nearer the cutting edge 82 serves as a chip breaker and also serves to increase the negative back rake of the cutting element with wear, which may be advantageous with some types of formation.

[0057] Figure 25 shows a similar arrangement, but in this case the insert 83 has a flat planar surface 84 to increase the back rake with wear.

[0058] Figure 26 is a front view of the basic preform cutting element formed with a circular aperture 85 ready to receive the inserts 77 or 83. The cutting element and insert may each be of any appropriate diameter. For example, the cutting element may be of 19mm diameter and the insert of 8mm or 13mm diameter, or the cutting element may be of 13mm diameter and the insert of 8mm diameter. The insert 77 or 83 may be brazed into the aperture 85 after the main part of the element has been bonded to the carrier 81.

[0059] The element shown in Figure 26 may also be used as a low cost cutter for a rotary drill bit by simply filling the aperture 85 with a cylindrical plug of tungsten carbide which may be brazed into place at the same time as the cutter 75 is brazed into the bit body. Such a cutter would, in use, achieve 39% wear before the wear flat reaches the carbide plug, rendering the cutter ineffective.

[0060] In any of the cutting elements according to the invention, the interface between the facing table and substrate may be non-planar and configured, instead of being substantially flat, so as to improve the bond between the facing table and substrate and also to provide other advantages, as is well known in the art. Alternatively or in addition, there may be provided between the facing table and the substrate a transition layer which may, for example, have certain characteristics, such as hardness, which are intermediate the corresponding characteristics of the facing table and substrate.

#### Claims

45

1. A preform cutting element for a rotary drag-type drill bit, comprising a front facing table of superhard material having a front surface, a peripheral surface, a rear surface bonded to a substrate of less hard material, and a cutting edge formed by at least part of the junction between the front surface and the peripheral surface, characterised in that the front surface of the facing table is formed with a formation which is located adjacent at least a part of the cutting edge and is shap d to deflect transversely of the front surface of the facing table cuttings which, in use, are removed by the cutting edge from the formation being drilled, th formation comprising at

10

30

35

40

50

55

least one protrusion which upstands from said front surface.

- A cutting element according to Claim 1, wherein the cutting element is circular or part-circular in shape.
- A cutting element according to Claim 2, wherein said formation extends around at least part of an outer marginal portion of the front surface of the facing table.
- A cutting element according to any of Claims 1 to 3, wherein the protrusion comprises a ridge formed on said front surface adjacent the cutting edge.
- A cutting element according to Claim 4, wherein the ridge has an outer edge which is spaced inwardly from the cutting edge.
- A cutting element according to Claim 5, wherein the outer edge of the ridge is spaced a substantially constant distance from the cutting edge.
- 7. A cutting element according to any of Claims 1 to 3, wherein the formation further comprises a groove formed in said front surface of the facing table adjacent the cutting edge, a portion of the front surface of the facing table between the groove and the cutting edge being configured to define said protrusions.
- A cutting element according to Claim 7, wherein the groove has an outer edge which is spaced inwardly from the cutting edge.
- A cutting element according to any of Claims 7, wherein the outer edge of the groove is spaced a substantially constant distance from the cutting edge.
- A cutting element according to any of Claims 7 to 9, wherein the groove is smoothly and concavely curved in cross-section.
- 11. A cutting element according to Claim 10, wherein the groove is part-circular in cross-section.
- A cutting element according to Claim 7 to 9, wherein the groove is V-shaped in cross-section.
- 13. A cutting element according to Claims 7 to 12, wherein there is formed in the groove a plurality of protrusions spaced apart longitudinally of the groove.
- 14. A cutting element according to Claim 13, wherein each protrusion has an upper surface which lies at substantially the same level as the front surface of

the facing table.

- A cutting element according to Claim 13 or Claim 14, wherein each protrusion extends transversely across the groove.
- 16. A cutting element according to Claim 15, wherein each protrusion extends across substantially the full width of the groove.
- 17. A cutting element according to any of Claims 13 to 16, wherein each protrusion is elongate and inclined at an angle of 90° to the length of the groove.
- 5 18. A cutting element according to any of Claims 13 to 16, wherein each protrusion is elongate and inclined at an angle of less than 90° to the length of the groove.
- 20 19. A cutting element according to Claim 18, wherein all the protrusions are inclined at substantially the same angle to the length of the groove.
  - 20. A cutting element according to Claim 18, wherein adjacent protrusions are inclined at opposite and equal angles to the length of the groove.
  - 21. A cutting element according to any of Claims 7 to 20, wherein said portion of the surface is formed with upstanding serrations.
  - 22. A cutting element according to Claim 21, wherein said serrations fill the space between the outer edge of the groove and the cutting edge, the cutting edge then being defined by parts of said serrations.
  - 23. A cutting element according to any of Claims 1 to 3, wherein the protrusion on the front surface of the facing table is provided by an insert which is received in a socket in the cutting element adjacent the cutting edge thereof, the insert including a part which is upstanding from the front surface of the facing table.
- 45 24. A cutting element according to Claim 23, wherein the insert and socket are substantially circular in cross-section.
  - 25. A cutting element according to Claim 23 or Claim 24, wherein at least the part of the insert which is received in the socket is cylindrical.
  - 26. A cutting element according to any of Claims 23 to 25, wherein the socket and insert extend through substantially the whole thickness of the cutting element.
  - 27. A cutting element according to any of Claims 23 to

6

26, wherein the upstanding part of the insert is domed.

- 28. A cutting element according to Claim 27, wherein the outer periphery of the dome lies at the same level as the front surface of the facing table.
- 29. A cutting element according to any of Claims 23 to 26, wherein the upstanding part of the insert has a front surface which is inclined away from the front surface of the facing table as it extends away from the cutting edge.
- **30.** A cutting element according to Claim 29, wherein the edge of said inclined surface nearest the cutting edge of the facing table lies at the same level as the front surface of the facing table.
- 31. A cutting element according to any of Claims 23 to 30, wherein the insert comprises a front layer of superhard material bonded to a substrate of less hard material, the superhard material forming the front surface of the upstanding part of the insert.

